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RESEARCH AND DEVELOPMENT OF WOUND DRESSING IN
MAXILLOFACIAL TRAUMA (U) BIOTEK INC WOBURN MA
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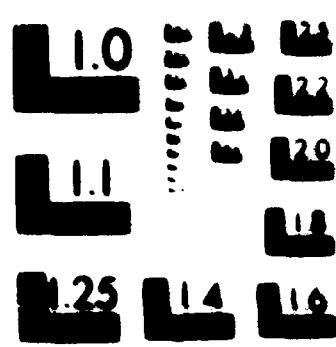
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Research and Development of wound Dressing
in Maxillofacial Trauma

Annual Summary Report

David L. Williams, Ph.D.
James H. Kerrigan, B.S.

April 1981

Supported by

U.S. ARMY MEDICAL RESEARCH AND DEVELOPMENT COMMAND
Fort Detrick, Frederick, Maryland 21701

Contract No. DAMD17-80-C-0091

Biotek, Inc.
Woburn, Massachusetts 01888

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in Maxillofacial Trauma

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Three kilograms of poly-L(-)lactide have been synthesized for this contract and for Contract No. DAMD 17-80-C-0110. This polymer has a viscosity (D₅) of 1.19 dl/g, a molecular weight (M_w) of 45,700 and a solvadversity of 1.4. Material from a previous contract was used for preliminary experiments.

Avitene mat has been obtained from FMC which can be used as a cellulose element for the non-woven fabric. Endone-melamine (EPM) resin is available and is insoluble in methylene chloride. Other trades include: starch, gelatin, etc.

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and also more readily cleared by the kidneys. However, a mixed solvent is required for material preparation.

Powders of polymer with lidocaine (HCl), etidocaine (HCl), benzocaine, and PVP-1, have been prepared using a hammer mill and dry ice. All composites contained 20% drug before and after comminution. Small particle sizes of powder containing the anesthetics released the drug rapidly. A 600-425 μ fraction containing 20% etidocaine released 20% of the drug in one hour, 40% in six hours, and 70% in 24 hours. Modifications of drug loading and drug form (e.g. free base, sulfate) are being considered.

PVP-1; is stable in the powder form, and 10% of the available iodine is found in the diffusion medium after one hour. However, a reaction occurs which removed iodine faster than it is released after the one hour measurement. This problem is under investigation.

Spraying a non-woven fabric of polymer and 20% lidocaine HCl caused corrosion of a copper tube. The equipment now has a spray gun (nickel plated), fluorocarbon gaskets, and glass and polyethylene connections. Fabric can now be produced; however, lidocaine diffusion is rapid from the present sample.

Samples of powder of each drug are being stored under six different conditions for stability studies.

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I. SUMMARY

Three kilograms of poly-L(-)lactide have been synthesized for this contract and for Contract No. DAAD 17-80-C-0110. This polymer has a viscosity (R.S.V.) of 1.19 dl/g., a molecular weight (M_w) of 45,700 and a polydispersity of 2.14. Material from a previous contract was used for preliminary experiments.

Avitene net has been obtained from FMC which can be used as a collection element for the non-woven fabric. Povidone-iodine (PVP-I₁) from Kapp Co is insoluble in methylene chloride. Other grades from BASF are more soluble and also more readily cleared by the kidneys. However, a mixed solvent is required for material preparation.

Powders of polymer with lidocaine (HCl), etidocaine (HCl), benzocaine, and PVP-I₁ have been prepared using a hammer mill and dry ice. All composites contained 20% drug before and after comminution. Small particle sizes of powder containing the anesthetics released the drug rapidly. A 600-425 μ m fraction containing 20% etidocaine released 20% of the drug in one hour, 40% in six hours, and 70% in 24 hours. Modifications of drug loading and drug form (e.g. free base, sulfate) are being considered.

PVP-I₁ is stable in the powder form, and 10% of the available iodine is found in the diffusion medium after one hour. However, a reaction occurs which removes iodine faster than it is released after the one hour measurement. This problem is under investigation.

Spraying a non-woven fabric of polymer and 20% lidocaine (HCl) causes corrosion of a copper tube. The equipment now has a spray gun (nickel plated), fluorocarbon gaskets, and glass and polyethylene connections. Fabric can now be produced, however, lidocaine diffusion is rapid from the present sample.

Samples of powder of each drug are being stored under six different conditions for stability studies.

II ACCOMPLISHMENTS

A. Drug Materials

The selection of drugs and polymer were based on the result of the screening of the previous contract. However, povidone-iodine was added to replace iodine, and collagen (Avitene^R) replaces gelatin (Gelfoam^R) as the hemostatic agent. Slow release of the hemostatic agent is neither required nor possible. Slow release of active iodine could be advantageous, if the wound remains open to infection. Slow release of the anesthetic is highly desirable.

1. Povidone-Iodine

The poly-L(-)lactide is soluble in methylene chloride and dioxane. Methylene chloride has been used in the previous contract for casting films and preparing non-woven fabrics. Iodine is soluble in methylene chloride, as is polyvinylpyrrolidone. However, the povidone-iodine complex is insoluble. This material was obtained from Kapp Chemical Company, but they have an exclusive arrangement with GAF for their supply. Only one grade of PVP-I₁ is available, although several molecular weights of PVP are available through GAF.

Several alternative suppliers of PVP-I₁ were contacted. Our first choice would be for low molecular weight PVP, secondarily, we could use a less iodinated material. Schenck, Simak, and Heedtke (1979) describe the povidone-iodine binding as an $\text{N}^+ - \text{I}_1^-$ complex. Several low molecular weight complexes were also made by this BASF group.

A second possibility is to use a mixed solvent for preparation of poly-lactide - PVP-I₁ materials. Methyl alcohol appeared to be the most probable second solvent for the drug and the polymer. A co-solvent for 10% polymer and 2% drug was needed. Therefore, a 15% polymer solution in methylene chloride was titrated with methanol and a 10% PVP-I₁ solution in methanol was titrated with methylene chloride. Considerable overlap exists and only a small quantity of methanol is required for PVP-I₁ solubility.

Letters were sent to nine suppliers of PVP-I. All of these suppliers are not necessarily manufacturers of the product. Samples were requested which could be tested for solubility in methylene chloride. A BASF Aktienoessellschaft sample (683-0493 Type 30/06) was received which had a greater solubility than the Rapp sample. However, it was significantly less than 2% soluble, which was our goal. Thus methanol was added to make a mixed solvent for particle composites of polymer and PVP-I. Very recently a PVP-I, Type 17/12 was received from BASF. This material complies with the Defense Medical Purchase Description (1/4/72). It is a low molecular weight material. This also conforms to the FDA concern on large wounds, only PVP-I should be used at all. The povidone portion can be eliminated from the body after possible resorption (BASF, 1980). The FDA considers this limit to be a molecular weight of 36,000. This is exceeded by less than 5% of the 17/12 material and about 50% of the standard K30 material. Based on this information we plan to use the BASF Type 17/12 for all future work. However, the material is also less than 2% soluble in methylene chloride.

In studying the literature on povidone-iodine (Schenck, Simak, and Heediche, 1979; Heel and Sobeille, 1981) absorption spectra were found. Therefore, an analysis at 290 nm was attempted for solubility and later drug release studies. Unfortunately Beer's law was not obeyed (absorption proportional to concentration), presumably because the complex dissociates at concentrations useful for spectrophotometry. Therefore, iodine has to be titrated with thiosulfate, as in the previous contract.

2 Incorporation of Avitene^B into Fiber Matrix

Avitene is a microfibrill collagen which is normally teased and collected with dry forceps. Avitene Corporation was contacted and John Tenery, M.C., states that they have made webs from either alcohol or air suspension of the Avitene fibrils. Aqueous media impair the effectiveness of the collagen. Dr. Tenery graciously sent 24 grams of Avitene for our experiments.

Hugo Stango, Ph.D., was contacted at FMC Corporation. They prepare a non-woven fabric mat using an air-laid device. They normally separate layers with glassine paper. The final product is approximately 1 mm thick, after being compressed about 6-fold. A sample of this material was graciously supplied by Fred Sorrells, Ph.D. of FMC.

Use of an FMC product as the collection element for the poly(lactide-drug) non-woven fabric appears to be the method of choice. However, a thinner and less dense Avitene mat would probably be quite adequate. The uncomressed material would also be more likely to collect and hold the polymer-drug fibers we are using gauze in our present experiments.

B Polymer Preparation

Poly-L(+)-lactide of a reduced viscosity of about 1.0 dl/g has been prepared and used by us for several government contracts. This was the polymer used for powder, film, and fabric preparation on the previous contract (DAMD 17-76-C-0019). It was also used for the preparation of lidocaine microcapsules by the surster process under Contract No. DAMD 17-79-C-9019. Finally, it is the polymer used for much of the steroid encapsulation work performed under Contract No. NAFW HE 32-78-1. The preparation of this polymer was described in detail in the annual report. The same method was used in the present contract.

The preparation of the poly(lactide) was performed as follows. The lactide dimer was obtained from Boehringer-Ingelheim through Henley and Company. This dimer was purified by repeated recrystallizations from ethyl acetate shortly before use. Reagent grade solvents were used for all operations. The lactide dimer was heated in a -10°C oil bath while stirring the melt, in vacuum, for 30 minutes to remove traces of volatile materials. Dry nitrogen was then introduced to release the vacuum. Next the bath temperature was raised to 180°C. To this mixture was added 0.2 ml of stannous octoate catalyst which is 6% in mineral oil. Within about 15 minutes after the catalyst addition, the polymer mixture reaches a maximum temperature. After about 30 minutes, the reaction is stopped by removing the mixture from the oil

bath, and the polymer is allowed to cool to room temperature. The polycaprolactone block is dissolved in methylene chloride and the solution is decanted and treated with three volumes of isopropanol, by slow addition to a stirred solution.

Two kilograms of poly-(L-)lactide which has a reduced specific viscosity (R.S.V.) between 1.0 and 1.5 dl/g are required for this contract. A parallel contract (DAMD 17-80-C-0110) also required an equivalent amount of polymer of the same R.S.V. To improve the characterization and reproducibility of both programs, it was decided to combine the requirements of both programs in one blend of a number of batches of polymer.

Approximately 1,200 grams of poly-(L-)lactide (R.S.V.=1.0 to 1.2 dl/g) was available from a previous contract (DAMD 17-79-C-9020). This material was used for preliminary experiments on both contracts to quantify operating parameters.

Because of the narrow range of the specified R.S.V. and the excessive heat generated in large batches, preparation of this quantity of polymer was a lengthy process. A total of 12 batches (see Table I) of dimer have been polymerized for these two contracts. Four of these were in the right range and eight were not. Five of the eight batches were too high and three were too low. Two of the out-of-range batches were exchanged with a similar project which had two batches which fell within our range but which were out of range for that application.

All six batches of polymer were blended together after dissolving in methylene chloride. A total of 19.3 liters of this polymer solution was precipitated by slow addition of isopropyl alcohol in the ratio of 3 to 1 (57.9 liters IPA). Due to the large volumes this had to be carried out in three batches.

TABLE I
POLYMERS USED FOR COMBINED PROGRAM

Polymer No.	Starting Grams <u>Dimer</u>	Approximate R.S.V
5-6-6	574	1.25'
5-6-10	649	1.02'
5-6-15	582	0.57'
5-6-18	600	2.91'
5-6-19	400	3.0
5-6-21	665	1.08'
5-6-23	617	3.0
5-6-25	637	2.23'
5-6-27	500	0.72'
5-6-29	500	2.08'
5-6-30	500	1.57'
5-6-31	300	0.92
7-12-2	500	1.40'
7-12-7	500	1.29'
 TOTAL	 7,524	

* used in blend (total of 3,300 gm)

* exchanged with NIM program for last two polymers or 15%

After precipitation, the polymer was removed from the solution by vacuum filtration. The cakes were pressed with rubber dam material in the Buchner funnel to remove most of the solvent. The polymer was then placed under vacuum to remove the residual solvent. Due to the low volatility of isopropanol and the large volume of polymer, the drying process took two weeks. When the polymer cakes were sufficiently dry, they were ground in a blender to a uniform size, shaken in a large bag and again placed under vacuum to complete the drying. Three random samples of this final mixture were taken and their viscosities determined in duplicate. The viscosity was found to be 1.9 ± 0.03 dl/g and the total weight obtained was 3,048 grams which was a 90% yield.

The polymer is presently being stored under argon in the freezer. The polymer was placed in plastic bags into one-gallon cans which are tightly sealed (paint cans). The air was removed by vacuum and replaced by argon, just prior to sealing. As mentioned in the proposal, this procedure has been standardized, but is presumably much more stringent than necessary to prevent polymer degradation.

A sample of polymer was sent to Cambridge Analytical Associates for determination of molecular weight distribution by gel permeation chromatography. Samples were dissolved in hot trichlorobenzene. Duplicate injections were run 12 hours apart to determine whether the hot temperature analysis would degrade the polymer. After 12 hours, no evidence of polymer degradation was evident. A series of μ -Styrene columns ($1, 10^1, 10^2, 10^3, 10^4$) from Waters Associates were used at 45°C . The flow rate was 1.5 ml/min and the change of refractive index was used for detection. The molecular weight determination was made by reference to polystyrene standards.

Data from the chromatograms of the polymer were reduced by standard methods. The results are shown in Table II. The weight average molecular weight of 45,700 is higher than expected for this viscosity of polymer (Kumayser, et al., 1976). However, provided other experiments are repeated with the same technique, any degradation can be quantified.

TABLE II
POLYMER MOLECULAR WEIGHT DISTRIBUTION

Sample	Polymer	Molecular Weight
	Number Ave. M_n	11,500
	Weight Ave. M_w	45,700
	M_w/M_n	4.0
	Polydispersity M_w/M_n	1.74

C. Fiber Mat Preparation

The fiber mat is being prepared in a manner similar to that of the previous contract work. About a 5% weight-to-volume solution of the polymer is prepared using methylene chloride as the solvent. The appropriate amount of drug is added to this system to obtain the appropriate drug/polymer ratio (e.g., 2%) This solution is poured into a tank which is connected to the liquid inlet of a Spraying Systems air atomizing nozzle using a piece of tubing.

The air inlet is connected to a tank of inert gas and the gas outlet pressure is set at about 4 psi. The polymer solution is fed into the nozzle body under gravity (e.g., 1 meter head) and fine polymer-drug fibers are formed as the solution leaves the nozzle. The fibers are collected on a piece of surgical gauze.

The previous method was reviewed with a representative of Spraying Systems Company. Materials were changed from stainless steel and rubber gaskets to nickel-plated brass and Teflon gaskets. An atomizing gun was obtained to facilitate shut-down. A clean-out needle assembly was included for the gun. Spraying nozzles are comprised of separate fluid and air caps, and all parts are readily interchangeable. Components were purchased for a round spray, as used previously (Set-up 2A) and two flat spray set-ups (F1 and F2C). The materials can also be assembled as Set-up 1 (see Table II B, which had also been used previously). The use of the gun, Teflon gaskets and flat spray head were significant improvements.

The Spraying Systems gun with appropriate nozzles was mounted, inverted, on a clamp. A straight 1.8" copper tube, one meter in length was attached to the fluid inlet. On top of this tubing was attached a series of gas pipe reducers. This formed a reservoir to give a constant hydrostatic head for spraying.

SPRAYING WITH A SPRAYING SYSTEM

SIPHON SPRAY SET UPS FOR 1:1 Round Spray

General shape and pattern of the round spray is maintained in section C. The liquid is maintained in section C by the liquid head. A, B, and D are the different widths of distances from nozzle to nozzle. D is the total distance of spray pattern. The width of spray pattern is double the distance between nozzles.

No.	Type of Nozzle Used	Flow rate of nozzle in gpm	Liquid capacity in one gallon per hour			Total distance of spray in feet
			1	2	3	
1	1/2" flat	1.0	100	200	300	100
2	1/2" flat	1.5	150	300	450	150
3	1/2" flat	2.0	200	400	600	200
4	1/2" flat	2.5	250	500	750	250
5	1/2" flat	3.0	300	600	900	300
6	1/2" flat	3.5	350	700	1050	350
7	1/2" flat	4.0	400	800	1200	400
8	1/2" flat	4.5	450	900	1350	450
9	1/2" flat	5.0	500	1000	1500	500
10	1/2" flat	5.5	550	1100	1650	550
11	1/2" flat	6.0	600	1200	1800	600
12	1/2" flat	6.5	650	1300	1950	650
13	1/2" flat	7.0	700	1400	2100	700
14	1/2" flat	7.5	750	1500	2250	750
15	1/2" flat	8.0	800	1600	2400	800
16	1/2" flat	8.5	850	1700	2550	850
17	1/2" flat	9.0	900	1800	2700	900
18	1/2" flat	9.5	950	1900	2850	950
19	1/2" flat	10.0	1000	2000	3000	1000
20	1/2" flat	10.5	1050	2100	3150	1050
21	1/2" flat	11.0	1100	2200	3300	1100
22	1/2" flat	11.5	1150	2300	3450	1150
23	1/2" flat	12.0	1200	2400	3600	1200
24	1/2" flat	12.5	1250	2500	3750	1250
25	1/2" flat	13.0	1300	2600	3900	1300
26	1/2" flat	13.5	1350	2700	4050	1350
27	1/2" flat	14.0	1400	2800	4200	1400
28	1/2" flat	14.5	1450	2900	4350	1450
29	1/2" flat	15.0	1500	3000	4500	1500
30	1/2" flat	15.5	1550	3100	4650	1550
31	1/2" flat	16.0	1600	3200	4800	1600
32	1/2" flat	16.5	1650	3300	4950	1650
33	1/2" flat	17.0	1700	3400	5100	1700
34	1/2" flat	17.5	1750	3500	5250	1750
35	1/2" flat	18.0	1800	3600	5400	1800
36	1/2" flat	18.5	1850	3700	5550	1850
37	1/2" flat	19.0	1900	3800	5700	1900
38	1/2" flat	19.5	1950	3900	5850	1950
39	1/2" flat	20.0	2000	4000	6000	2000
40	1/2" flat	20.5	2050	4100	6150	2050
41	1/2" flat	21.0	2100	4200	6300	2100
42	1/2" flat	21.5	2150	4300	6450	2150
43	1/2" flat	22.0	2200	4400	6600	2200
44	1/2" flat	22.5	2250	4500	6750	2250
45	1/2" flat	23.0	2300	4600	6900	2300
46	1/2" flat	23.5	2350	4700	7050	2350
47	1/2" flat	24.0	2400	4800	7200	2400
48	1/2" flat	24.5	2450	4900	7350	2450
49	1/2" flat	25.0	2500	5000	7500	2500
50	1/2" flat	25.5	2550	5100	7650	2550
51	1/2" flat	26.0	2600	5200	7800	2600
52	1/2" flat	26.5	2650	5300	7950	2650
53	1/2" flat	27.0	2700	5400	8100	2700
54	1/2" flat	27.5	2750	5500	8250	2750
55	1/2" flat	28.0	2800	5600	8400	2800
56	1/2" flat	28.5	2850	5700	8550	2850
57	1/2" flat	29.0	2900	5800	8700	2900
58	1/2" flat	29.5	2950	5900	8850	2950
59	1/2" flat	30.0	3000	6000	9000	3000
60	1/2" flat	30.5	3050	6100	9150	3050
61	1/2" flat	31.0	3100	6200	9300	3100
62	1/2" flat	31.5	3150	6300	9450	3150
63	1/2" flat	32.0	3200	6400	9600	3200
64	1/2" flat	32.5	3250	6500	9750	3250
65	1/2" flat	33.0	3300	6600	9900	3300
66	1/2" flat	33.5	3350	6700	10050	3350
67	1/2" flat	34.0	3400	6800	10200	3400
68	1/2" flat	34.5	3450	6900	10350	3450
69	1/2" flat	35.0	3500	7000	10500	3500
70	1/2" flat	35.5	3550	7100	10650	3550
71	1/2" flat	36.0	3600	7200	10800	3600
72	1/2" flat	36.5	3650	7300	10950	3650
73	1/2" flat	37.0	3700	7400	11100	3700
74	1/2" flat	37.5	3750	7500	11250	3750
75	1/2" flat	38.0	3800	7600	11400	3800
76	1/2" flat	38.5	3850	7700	11550	3850
77	1/2" flat	39.0	3900	7800	11700	3900
78	1/2" flat	39.5	3950	7900	11850	3950
79	1/2" flat	40.0	4000	8000	12000	4000
80	1/2" flat	40.5	4050	8100	12150	4050
81	1/2" flat	41.0	4100	8200	12300	4100
82	1/2" flat	41.5	4150	8300	12450	4150
83	1/2" flat	42.0	4200	8400	12600	4200
84	1/2" flat	42.5	4250	8500	12750	4250
85	1/2" flat	43.0	4300	8600	12900	4300
86	1/2" flat	43.5	4350	8700	13050	4350
87	1/2" flat	44.0	4400	8800	13200	4400
88	1/2" flat	44.5	4450	8900	13350	4450
89	1/2" flat	45.0	4500	9000	13500	4500
90	1/2" flat	45.5	4550	9100	13650	4550
91	1/2" flat	46.0	4600	9200	13800	4600
92	1/2" flat	46.5	4650	9300	13950	4650
93	1/2" flat	47.0	4700	9400	14100	4700
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95	1/2" flat	48.0	4800	9600	14400	4800
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98	1/2" flat	49.5	4950	9900	14850	4950
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100	1/2" flat	50.5	5050	10100	15150	5050
101	1/2" flat	51.0	5100	10200	15300	5100
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103	1/2" flat	52.0	5200	10400	15600	5200
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105	1/2" flat	53.0	5300	10600	15900	5300
106	1/2" flat	53.5	5350	10700	16050	5350
107	1/2" flat	54.0	5400	10800	16200	5400
108	1/2" flat	54.5	5450	10900	16350	5450
109	1/2" flat	55.0	5500	11000	16500	5500
110	1/2" flat	55.5	5550	11100	16650	5550
111	1/2" flat	56.0	5600	11200	16800	5600
112	1/2" flat	56.5	5650	11300	16950	5650
113	1/2" flat	57.0	5700	11400	17100	5700
114	1/2" flat	57.5	5750	11500	17250	5750
115	1/2" flat	58.0	5800	11600	17400	5800
116	1/2" flat	58.5	5850	11700	17550	5850
117	1/2" flat	59.0	5900	11800	17700	5900
118	1/2" flat	59.5	5950	11900	17850	5950
119	1/2" flat	60.0	6000	12000	18000	6000
120	1/2" flat	60.5	6050	12100	18150	6050
121	1/2" flat	61.0	6100	12200	18300	6100
122	1/2" flat	61.5	6150	12300	18450	6150
123	1/2" flat	62.0	6200	12400	18600	6200
124	1/2" flat	62.5	6250	12500	18750	6250
125	1/2" flat	63.0	6300	12600	18900	6300
126	1/2" flat	63.5	6350	12700	19050	6350
127	1/2" flat	64.0	6400	12800	19200	6400
128	1/2" flat	64.5	6450	12900	19350	6450
129	1/2" flat	65.0	6500	13000	19500	6500
130	1/2" flat	65.5	6550	13100	19650	6550
131	1/2" flat	66.0	6600	13200	19800	6600
132	1/2" flat	66.5	6650	13300	19950	6650
133	1/2" flat	67.0	6700	13400	20100	6700
134	1/2" flat	67.5	6750	13500	20250	6750
135	1/2" flat	68.0	6800	13600	20400	6800
136	1/2" flat	68.5	6850	13700	20550	6850
137	1/2" flat	69.0	6900	13800	20700	6900
138	1/2" flat	69.5	6950	13900	20850	6950
139	1/2" flat	70.0	7000	14000	21000	7000
140	1/2" flat	70.5	7050	14100	21150	7050
141	1/2" flat	71.0	7100	14200	21300	7100
142	1/2" flat	71.5	7150	14300	21450	7150
143	1/2" flat	72.0	7200	14400	21600	7200
144	1/2" flat	72.5	7250	14500	21750	7250
145	1/2" flat	73.0	7300	14600	21900	7300
146	1/2" flat	73.5	7350	14700	22050	7350
147	1/2" flat	74.0	7400	14800	22200	7400
148	1/2" flat	74.5	7450	14900	22350	7450
149	1/2" flat	75.0	7500	15000	22500	7500
150	1/2" flat	75.5	7550	15100	22650	7550
151	1/2" flat	76.0	7600	15200	22800	7600
152	1/2" flat	76.5	7650	15300	22950	7650
153	1/2" flat	77.0	7700	15400	23100	7700
154	1/2" flat	77.5	7750	15500	23250	7750
155	1/2" flat	78.0	7800	15600	23400	7800
156	1/2" flat	78.5	7850	15700	23550	7850
157	1/2" flat	79.0	7900	15800	23700	7900
158	1/2" flat	79.5	7950	15900	23850	7950
159	1/2" flat	80.0	8000	1		

It was decided to use Parke-Davis sterile gauze as backing material to spray the polymer. This material is held at a fixed distance from the gun nozzle and is attached to an embroidery hoop to keep it flat. Thus air passes through the wound dressing to facilitate drying of the solvent.

A 10% polymer solution in methylene chloride was made with previously synthesized polymer (#70-74) which had a recently measured viscosity (R.S.V.) of 1.18 dl/g. The Spraying Systems atomizing gun (nickel plated brass with teflon gaskets) with various combinations of air caps and fluid caps was tried at various pressures. In all cases the nozzles plugged either immediately or shortly after the spraying started.

The 10% solution was diluted with methylene chloride to 5% and to 2.5%. The 2.5% continued to spray but did not deposit much material on the gauze. The 5% polymer solution was used with various combinations of air caps, fluid caps, air pressure, and distances of gauze from the nozzle. Table I.

Using 5% polymer solution with fluid cap 2850 and air cap 73420 (flat spray setup #1 in catalogue), the nozzle clogged after some collection at 1 psi and immediately at 3.75 psi pressure. At 2.5 psi, fiber was collected at 22 cm from the nozzle.

In another combination, fluid cap 2850 was used with air cap 70 (round spray). This setup (#2 in the catalogue) was tested at 2.5 and 5 psi at distances of 22, 30, and 38 cm from the nozzle. All runs with the round spray air cap gave fabric that looked like films with varying amounts of shot (Table IV).

Based on the results of the preliminary runs the best fibers were produced with the flat spray air cap No. 73420 and the fluid cap No. 2850 using a 5% polymer solution. These fabrics appear similar to those prepared under the previous contract.

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<u>Microscopic Evaluation</u>	<u>Air Gap</u>	<u>Distance from Nozzle</u> <u>(cm)</u>	<u>Air Pressure</u> <u>(psi)</u>	<u>Comments</u>
1 mm with holes	70	22	5	Closed soon
Mostly fibers/ some shot	70	22	5	
Mostly shot/ some fibers	70	22	2.5	
A few fibers (little product)	70	22	3.75	Closed immediately
Mostly shot/ some fibers	70	20	2.5	
Some shot and some fibers	70	20	5.0	
Mostly shot	70	20	5.0	

When the final contract polymer became available, the system was re-evaluated using 20% lidocaine (HCl) with 80% polymer. The system was modified to measure air flow rather than tank pressure. Samples are better prepared in a laboratory hood. When the hood is on the air draft pulls air through the fabric and also affects the overall spray pattern.

The results are shown in Table V. In the first series of tests with lidocaine-HCl (101-104), the fabric turned green with time indicating a leaching of the copper. The copper was replaced with polyethylene tubing and a glass (separatory) funnel. The lidocaine (HCl)-polymer fabric is now white again. From several of these tests it appears that low polymer (and drug) concentrations produce a low density product. However, this product is primarily discreet particles, similar to snow or whitened cream. High polymer concentrations produce more fibrous material. However, film formation and nozzle plugging can occur. Less film formation occurs as the distance from nozzle to collector increases.

All of the recent samples have been photographed and catalogued. For comparison, photomicrographs of a fibrous (409) and non-fibrous (301) samples are shown in Figure 1. A sample of material (409) is attached as Figure 2. The photographs are deceiving because of the lack of depth of field. Sample 409 has been sent to Col. Tsaknis (USAIDR) for scanning electron microscopy.

D. Powder Preparation

In the previous contract work, powders were prepared by comminution of material prepared as a film, by grinding at liquid nitrogen temperature. Both mortar and pestle and micro-mill apparatus was employed. Since these methods cannot be readily scaled up to common pharmaceutical equipment, different methods were employed in this contract work.

TABLE I
FABRIC PREPARATION USING 20% LIDOCAINE HCl IN POLYMER
 (Fluid Cap 2850, Air Cap 70)

<u>Test No.</u>	<u>Charge g/l Polymer</u>	<u>Soln Hood in</u>	<u>Gas Flow SCFH</u>	<u>Nozzle to Collector cm</u>	<u>Hood Off On</u>	<u>Spray Continuous Intermittent Stationary Moving</u>
101	30	5	1.1	50	30	• 0
102	30	5	1.1	20	30	• •
103	•	5	1.1	30	45	• •
104	50	5	1.1	50	45	• •
201	30	5	1.1	25	33	• •
202	30	5	1.1	35	47	• •
203	30	5	1.1	30	53	• •
204	•	5	1.1	20	40	• •
205	30	5	1.1	10	40	• •
206	30	5	1.1	15	50	• •
207	30	5	1.1	20	55	• •
208	30	5	1.1	20	40	• •
209	30	5	1.1	20	55	• •
210	50	2.5	1.1	20	55	• •
211	50	2.5	1.1	30	40	• •
301	30	5	1.0	20	50	• •
302	•	5	1.0	40	50	• •
303	100	2.5	1.5	40	50	• •
304	•	2.5	1.5	60	75	• •
401	50	10	1.5	40	30	• •
402	•	10	1.5	60	75	• •
403	•	10	1.5	60	75	• •
404	50	10	1.5	30	90	• •
405	50	10	1.5	30	90	• •
406	50	10	1.5	30	90	• •
407	50	10	1.5	30	45	• •
408	•	10	1.5	40	60	• •
409	•	10	1.5	40	75	• •

* continuation of same charge



A
Particulate Form 301



B
Fibrous Mat 409

FIGURE 1 PHOTOMICROGRAPH OF NON-WOVEN FABRIC CONTAINING 20%
LIDOCAINE HCl

FIGURE 2 SAMPLE OF NON-WOVEN FABRIC SHOWN IN FIGURE 1B

Since the previous powders which showed good drug delivery had sizes of 50 to 250 microns, it was important to maintain this approximate size distribution. Thus micronization in a fluid energy mill would presumably not be advantageous.

Felmetster (1970) describes the common apparatus and methods of producing powders for the pharmaceutical industry. Of the intermediate pulverizers described, the hammer mill is the most applicable to the present materials. He, therefore, sent samples of films to Dr. S.B. Roy at Massachusetts College of Pharmacy (Boston, MA) for hammer milling under cold conditions. A cooled mill would be most appropriate for large scale production. For small scale production the sample was sent through a standard mill with dry ice.

Solutions of 20 grams of drug and 80 grams of polymer were prepared using 700 ml of methylene chloride. For povidone-iodine 20 grams of Kapp povidone-iodine (USP, Lot 9124) was dissolved with 80 grams of polymer, using 800 ml of methylene chloride and 40 ml of methanol. Films were cast into seven flat glass vessels of 400 cm² area, and hence the average thickness was about 360 μ m. These films were cut with scissors into squares of approximately 5 x 5 mm. These pieces could be fed with the sugar into the hammer mill.

A Micro-Pulverizer C.F. (18,000 RPM, Pulverizing Machinery, Div. Stich Industrial Co., Summit, N.J.) was used. The mill was assembled with the hammer edge of the rotor facing the direction of rotation. A 20 mesh (841 μ m) classifier screen was used at the bottom of the mill. The feed and comminution chamber were pre-cooled with 500 grams of dry ice. Next the sample was sent through the mill, sized 1 to 10 with dry ice (i.e., 90° C.O.). A final charge of 100 grams of dry ice was sent through the mill to increase the yield from the chamber. The mill was dismantled, washed, dried, and re-assembled for each drug run.

The resulting powders were sieved with the Sonic Sifter at BIOTEC and the results are shown in Table VI.

TABLE VI
PERCENT OF POWDER IN VARIOUS SIZE FRACTIONS
(20% drug)

<u>Size (μm)</u>	<u>Lidocaine</u>	<u>Etidocaine</u>	<u>Benzocaine</u>	<u>Povidone-Iodine</u>
600	17.7	9.0	1.1	11.7
600-425	28.5	27.0	27.1	46.1
425-300	7.0	5.5	18.8	9.9
300-212	9.4	10.9	13.1	7.0
212-150	13.2	17.1	12.5	7.4
150-106	13.6	15.1	17.0	7.5
106-74	3.0	12.1	4.7	3.9
74-50	4.1	3.1	4.4	6.0
< 50	0.2	0.2	0.2	0.2
Milling Recovery	683	678	893	862

E. Drug Release Studies

1. Method of Measurement

Drug release is measured in a manner similar to the previous contract work. Ultraviolet absorption is used to measure the amount of anesthetic released and a titration is used to measure the amount of available iodine released from povidone-iodine. A known area of non-woven fabric is cut (17 mm diameter, 2.27 cm²), and the sample is weighed after removing the fabric backing. Powders of various size ranges are weighed out directly. These samples are placed in 44 µm mesh heat-sealed bags. These sample bags are then placed in L-shaped diffusion cells to which 40 ml of pH 7.4 phosphate buffer has been added. Good mixing is assured and the temperature is maintained at 37°C in this system. As in the previous work, solutions are analyzed after 1, 2, 4, 6, and 24 hours of sample contact. Fortunately all of these drugs are quite soluble and relatively stable in this buffer. As in the previous contract work, etidocaine samples are acidified before being measured by ultraviolet absorption. Also, as in the previous contract, iodine is analyzed by titration with sodium thiosulfate, using a starch end point for the diffusion sample.

Standard curves are generated from the pure drugs and a least-squares equation is used for determining drug weights. Calculations, involving assay values and sample loss due to etidocaine acidification, are performed by computer. Drug assays are performed in methylene chloride, using a calibration curve in the same solvent.

2. Powder Assays

As expected, drug assays of particles were identical to the initial 20% drug loading for the anesthetics. This was true regardless of particle size. For povidone-iodine-polymer particles, some degradation may occur. Instead of 20.0%, 18.73 was recovered using a thiosulfate titration procedure in 50/50 CH₂Cl₂/CH₃OH.

3. Powder Release Studies

The drug release results of the first set of milled particles are shown in Table VII. Since most of the available drug was released in the first hour, the data for 2, 4, 6, and 24 hours is practically identical. Hence only the 1 and 24 hour data are tabulated. In this test, using a sample submerged in moving buffer, release is too fast for delayed drug action. Drug release is faster than observed in the previous contract work for etidocaine and benzocaine. Larger size particles will be tested since it is possible that the slow release in the previous work was due to a few large particles in the unsieved powder. In a recent test, the hypothesis was confirmed that larger particles would release drugs significantly more slowly. A sample of 425 to 600 μm powder was studied and the results are shown in Figure 3.

Comparing iodine samples of the previous contract with the present doxidone-iodine samples, PVP-I₂ is much more stable. Iodine from PVP-I₂ is not released to the air, discoloring even the sample containers. PVP-I₂ does not appear to react significantly with poly lactide during film and powder formation. However, a loss of available iodine during the release studies remains unexplained. An assay titration of the spent particles (after release study) showed no significant residual iodine in the particles.

It may be unnecessary to have a slow release of antiseptic agents such as PVP-I₂. Iodine kills bacteria instantly on contact (Bogash, 1956), and PVP-I₂ releases active iodine within milliseconds after dissolution (Schlezinger, Matzke, and Levin, 1979). Once a wound is antiseptic and bandaged, continued release of antiseptic agent may be unnecessary. However, it is important that active iodine be released from the wound dressing. We, therefore, propose studies to measure release of active iodine by addition of soluble starch to the solution (Schlezinger, et al., 1979) and determination of bactericidal effectiveness of the wound dressings.

TABLE VII
PERCENT DIFFUSION OF SMOKE IN ONE HOUR OR ONE DAY

Particle Size (μ)	Cigarette per Day	Smoking per Day	Penicocaine Hour Day	Penicocaine Day	Penicocaine - Loading Hour	Penicocaine - Loading Day	
100-212	67	80	44	150	41	59	10.5
212-350	75	79	36	56	32	68	6.0
350-1000	65	69	49	60	31	48	10.7
1000-214	69	71	73	76	37	52	9.0
214-350	64	71	71	71	30	50	12.0

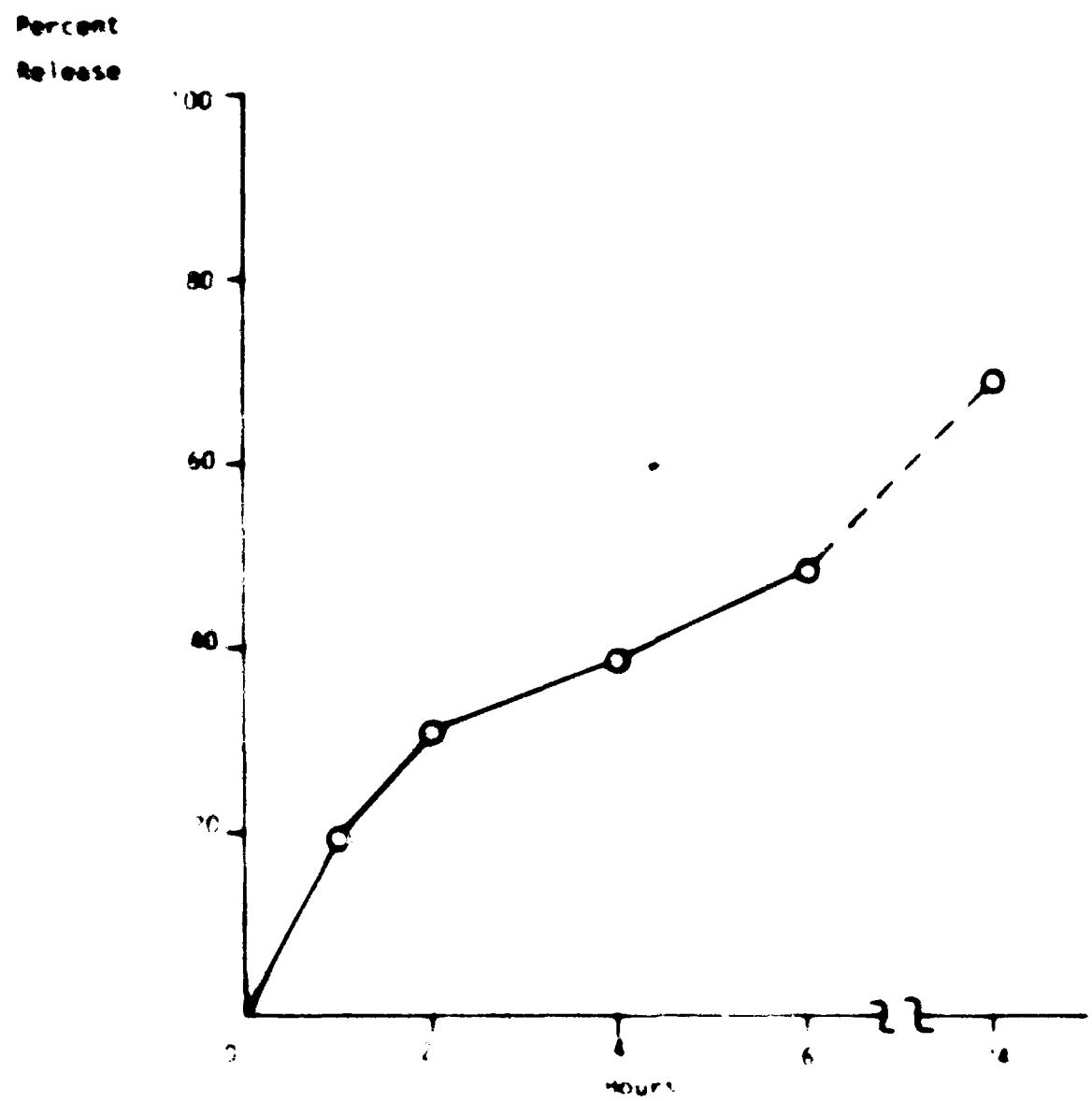


FIGURE 1. LIDOCAINe RELEASE FROM 400 MG 42% ESRD TABLETS

Iodoctaine particles were washed with various solutions and dried. In an attempt to eliminate the initial burst of drug release, a 5-minute water rinse was attempted which should dissolve the drug on the outside of the particles. Unfortunately this water rinse removed 82% of the drug. A diffusion analysis on the remainder of the drug was inconclusive. Five minute rinses with 0.1 N NaOH, 0.1 N Na₂SO₄, and 0.05 M phosphate buffer (pH 7.4) were performed in an attempt to precipitate the drug on the outside of the particle. The base form of lidocaine and the sulfate and phosphate forms are less soluble than the hydrochloride. Again the water removed most of the drug (78-84%), and an analysis of the remaining drug release was inconclusive. Slower release is more likely to be achieved by preparing new samples which incorporate these less soluble drug forms in the polymer matrix, and/or by preparing samples which have lower drug loadings.

E Fabric Release Studies

Only preliminary studies have been performed on lidocaine-polymer non-woven fabric. No significant (> 1 hour) delayed release was observed.

F Sample Storage

Particles of 300 to 212 μ m of lidocaine, etidocaine, benzocaine, and povidone-iodine have been prepared for storage under the six conditions which were proposed (Table VIII). Two separate containers of each drug are being prepared. One container will be opened at the end of the contract year for assay and release testing. The other container holds twice as much material and will be held for two later analyses. American Can Company has previously supplied sufficient M-1173 61-0 93004 heat-sealable bags for dessicant storage. Pouches consist of Bertuf Poly/Foil/L D.P.E. Ambient moisture is achieved in bottles capped with glass wool. Absence of light is achieved with black tape. Temperatures are 40°C (chemical oven), ambient (laboratory), 4°C (refrigerator).

TABLE VIII
SAMPLE STORAGE CONDITIONS

<u>CONDITION</u>	<u>TEMPERATURE</u>	<u>HUMIDITY</u>	<u>LIGHT</u>
1	40°C	Ambient	None
2	40°C	Desiccate	None
3	Ambient	Ambient	None
4	Ambient	Ambient	Ambient
5	4°C	* Ambient	None
6	4°C	Desiccate	None

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